

SUPPLY QUALITY IMPROVEMENT USING SERIES COMPENSATOR

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ABSTRACT

This paper introduces a variable capacitive reactance for compensation using a series controlled capacitor for load voltage stabilization. Employing capacitors is the simplest method of reducing the effective impedance the line. The proposed system operates for load voltage stabilizing with static or dynamic load. This system improves input power factor and reduces the input line current harmonic. The proposed system is used also for mitigation of voltage sag. Simulation and experimental results are obtained for open and closed loop voltage control system. The integral proportional (PI) controller is used to control the load voltage by controlling the capacitor effect. The effectiveness of the proposed method is verified through simulation and experimental results.

Keywords: Load voltage, series compensation, Voltage sag

1. INTRODUCTION

The recent developed of semiconductor device technology realizes small size, light-weight, and high performance power switching device. But reactive elements such as an inductor or capacitor are still physically large and heavy. If a compact and high efficient reactive component is developed, the power converter technology may drastically change the application field [1-2].

The series controlled capacitor consists of an inverter and capacitor; this system can produce larger value of a reactance than actually used, the value of the virtual reactance can be varied [3]. Using controlled capacitor and/or inductor can generate not only positive inductance which exists naturally, but can also produce negative reactance that cancels undesired inductance including in transient state of the system. Negative inductance can decrease the circuit impedance without any additional resonance [4].

Use of capacitors is the simplest method of reducing the effective impedance of a line. Control is affected by switching capacitors into or out of load circuit. Use of series capacitors calls for special protection schemes and may caused instabilities due to the formation of resonant circuits in combination with inductances naturally present in a network [5].

In order to improve the supply quality and power factor, controlled capacitor used in series with inductive load (static or dynamic). In this paper a

variable reactance type series compensation by using a series controlled capacitor is proposed to operate as an ac voltage controller for controlling the load voltage, without any discontinuity in the supply current, also it can operate as a boost ac chopper, when the capacitor reactance is greater than the circuit inductive reactance. Using controlled capacitor in the proposed system improves the supply quality and the transient performance of the dynamic loads [6].

A voltage sag is a reduction between 10 and 90% in root-mean-square voltage, with a duration between 0.5 cycles and 1 min. It is generally caused by a short circuit or overload in the utility system, also, due to starting of heavy induction motors. Typically, voltage sag duration ranges from 0.5 to 30 cycles, and its depth depends on the power system distribution and the approximately to the fault site [7]. Adjustable-speed drives (ASDs) are one of the most sensitive loads to voltage sags because transient voltages cause nuisance tripping events [8]. The mitigation of voltage sag is introduced in many paper [9-11].

In this paper the proposed system with insertion technique is used for mitigation of voltage sag, also the load voltage can be stabilized over a wide range taking the supply impedance into account

2. SYSTEM DESCRIPTION

The proposed system of series controlled capacitor for load voltage stabilization is shown in Figure (1).

In this system, the supply impedance is taken into account, and the load may be inductive (static or dynamic).

Series controlled capacitor is used to decrease the effect of load and supply inductances, without any discontinuity in the supply current. The effective value of the capacitor can be controlled from zero to maximum value through four IGBT's. Analog drive circuit is built to generate two groups of pulses for controlling the IGBT's, where each pair of IGBT's is switched alternatively. Control voltage will control the duty cycle of pulses to control the capacitor current.

The system can be operate at lagging power factor ($x_t > x_c$), with low duty ratio, or at leading power factor ($x_t < x_c$), with high duty ratio.

Where, X_t is the total equivalent series inductance of the load and supply.

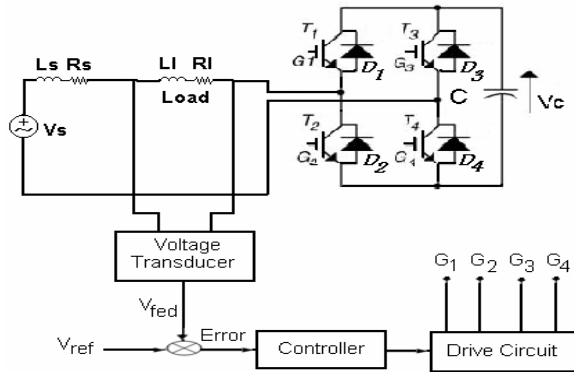


Figure (1) The proposed system for load voltage stabilization

3. SYSTEM MODELING

Considering R-L load, the drive circuit generates two groups of pulses, where each pair of IGBT's is switched alternatively. During positive half cycle, the switches (T_2, T_3) are forward biased and switches (T_1, T_4) are reverse biased. Differential equations for each mode of operation (in positive half cycle) can be written as follows:

3.1 Mode (1)

In this mode, when switches (T_2, T_3) are turned on. The current flows taking the path shown in Figure (2), and the capacitor C is connected to the line circuit where the capacitor will be charging. The corresponding differential equations describing this mode are;

$$V_s = i \cdot R_t + L_t \cdot \frac{di}{dt} + V_c \quad (1)$$

$$V_c = \frac{1}{c} \cdot \int i \cdot dt \quad (2)$$

3.2 Mode (2)

This mode starts when the switches (T_2, T_3) are off. The current will be following in the same direction as

in mode (1) because the inductance of the circuit, so the current will be passes in the two diodes (D_1, D_4). So the polarity of the capacitor will be reversed, and the capacitor voltage will be discharged. The current flows taking the path shown in figure (3). The corresponding differential equations describing this mode are as follows:

$$V_s = i \cdot R_t + L_t \cdot (di / dt) - V_c \quad (3)$$

During negative half cycle, the same two modes which shown above are repeated but through T_1, T_4 (charging), and D_2, D_3 discharging.

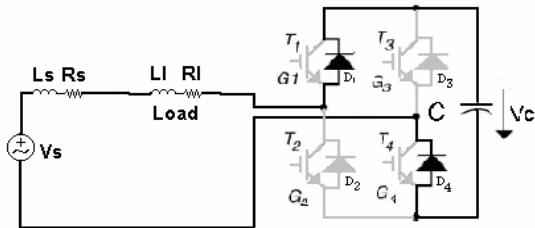


Figure (2) Equivalent circuit of mode 1 of operation during positive half cycle

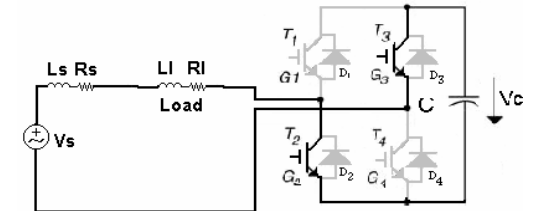


Figure (3) Equivalent circuit of mode 2 of operation during positive half

4. CLOSED LOOP LOAD VOLTAGE CONTROL

The load voltage is affected by switching capacitor into or out of load circuit. The closed loop with PI controller is used for stabilizing the load voltage as shown by block diagram in figure (4).

The feed back voltage is compared with the reference voltage. Error is fed to the integral unit to give signal U that compared with the same feed back voltage, the result signal is fed to the proportional unit. The control voltage is responsible for changing the duty ratio of switches operation to control the capacitor value that stabilizes the load voltage at the value corresponds to the reference voltage. The controller equation can be written as:

$$\tau_1 \cdot (du / dt) = V_{ref} - K_v \cdot V_L \quad (4)$$

$$V_c = K_1 (U - K_v \cdot V_L) \quad (5)$$

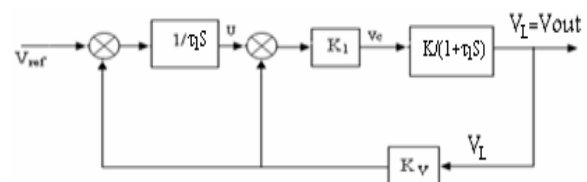


Figure (4) PI Controller Block Diagram

5. SIMULATION AND EXPERIMENTAL RESULTS

The results of the proposed system with static load are taken for open and closed loop. The simulation results of the system for open and closed loop are obtained using MATLAB software. Experimental results of the system for open and closed loop are obtained using a laboratory set-up of the proposed system (Appendix), where analogue circuits of PI controller and drive circuit of the switches are built and tested.

5.1. Open Loop System

Figure (5) shows the simulation and experimental waveforms of the supply voltage and current at $V_S=60$ volt and duty ratio=75%. It is noticed that the supply current is nearly sinusoidal without any discontinuity. Changing the duty ratio of the switches operation will change the current waveforms.

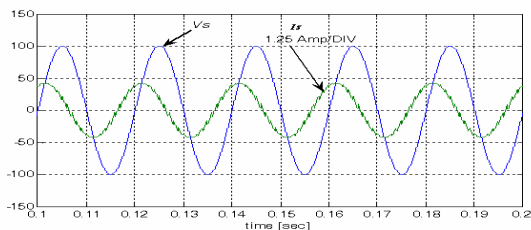
Figure (6) shows the simulation and experimental waveforms of the load voltage at $V_S =60$ volt and duty ratio=75%.

Figure (7) shows the relation between duty ratio and the input power factor. It is clear that, increasing the duty ratio increases the input power factor.

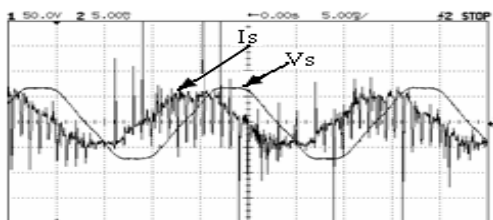
5.2. Closed-Loop System with (PI) Voltage Controller

Figure (8) shows the simulation and experimental results of load voltage due to + 25% change in reference voltage. It is clear that, the load voltage follows the desired reference voltage.

Figure (9) shows the simulation and experimental results of load voltage and load current due to 15% step change in the load. It is noticed that, during step change in the load by increasing or decreasing the load current within certain limits + 15% of the full load value, the proposed system will keep the load voltage constant as shown in figure (9).

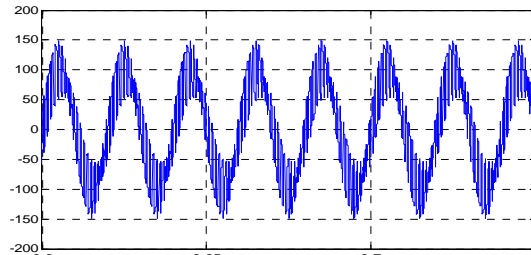


(a) Simulation

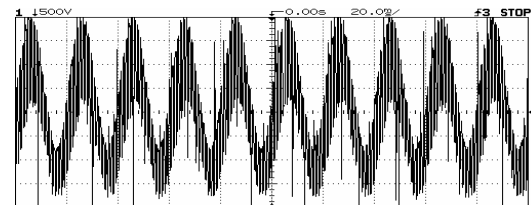


(b) Experimental

Figure (5) Simulation and experimental results of supply voltage and current at $V_S=60$ Volt and duty ratio = 75%



(a) Simulation



(b) Experimental

Figure (6) simulation and experimental results of load voltage at $V_S= 60$ Volt and duty ratio = 75%

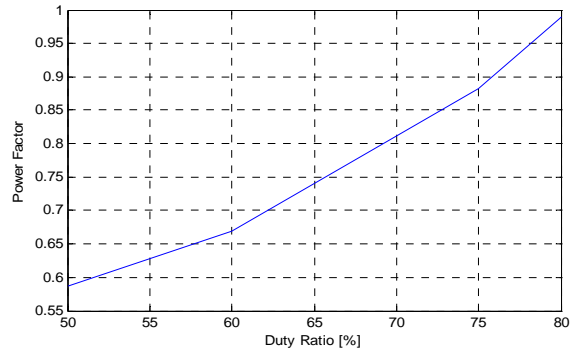
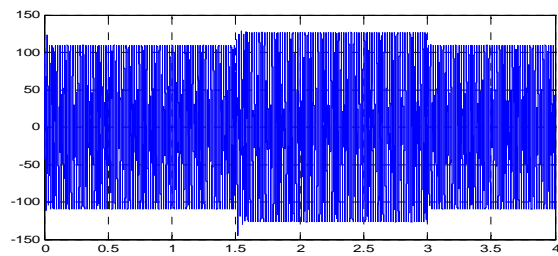
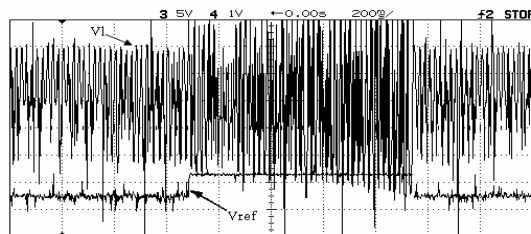


Figure (7) The relation between duty ratio and the input power factor



(a) Simulation



(b) Experimental

Figure (8) Simulation and Experimental results of load voltage due to + 25% change in reference voltage

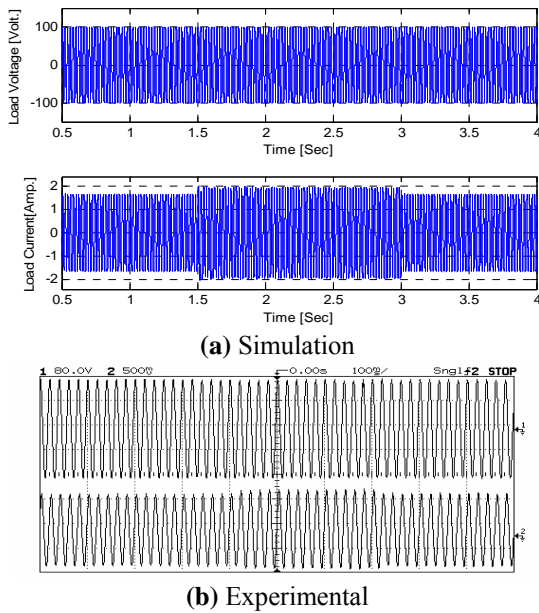


Figure (9) simulation and experimental results of load voltage and load current due to + 15% step change in the load

6. VOLTAGE SAG MITIGATION

Voltage sag is one of the main power quality problems faced by many industrial customers. It is a reduction between 10 and 90% in root-mean-square voltage, with a duration between 0.5 cycles and 1 minute that may be accompanied with phase jumps and are caused by faults on the power system or starting large loads, such as motors. Equipment used in modern industrial plants (process controllers, programmable logic controllers, adjustable speed drives, and robotics) is becoming more sensitive to voltage sag due to the increased complexity of the equipment. Voltage sag causes sensitive equipment to trip and this can result in considerable financial losses experienced by the industrial customers.

There are different techniques to overcome voltage sag such that; Tap Changers ; Thyristor-Controlled Reactor (TCR); Thyristor-Switched Capacitor (TSC); Dynamic Voltage Restorer (DVR) [12-16].

The proposed system shown in Figure (10) is used for voltage sag mitigation. The load is ac motor in system 1. The load voltage is changed by changing the injected voltage by controlling the duty ratio of the switches in system 2, so the load voltage can be kept at constant value, where the duty ratio is employed to vary the equivalent reactance seen by the transmission line at the transformer primary winding. Prototype had been built and tested to check the idea of voltage sag mitigation.

6.1. Run-Up Characteristics

Figure (11) shows the experimental results for the load voltage and current during Run-up without insertion, but Figure (12) shows the experimental

results for the load voltage and current during Run-up with insertion. It is noticed that, in figure (11) there is a voltage dip in load voltage during starting due to the large starting current of the motor; but in Figure (12) the load voltage and current are constant during the starting due to using the proposed technique of insertion from system 2.

Note, the scale in figure (11) is increased by percentage 1:10 by using resistance.

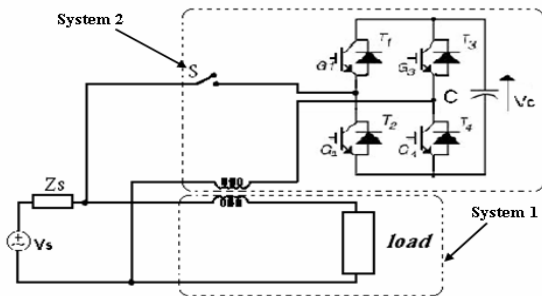


Figure (10) The proposed system for voltage sag mitigation

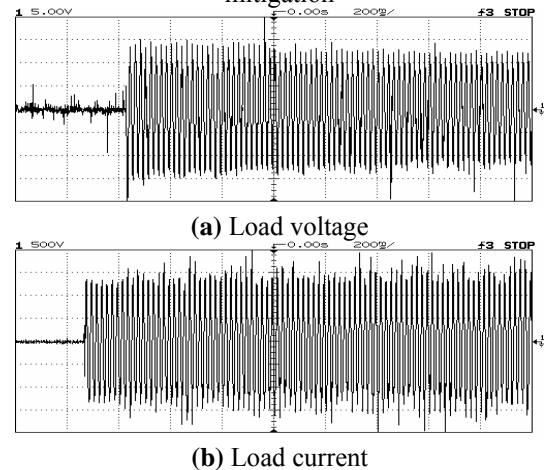


Figure (11) load voltage and current during Run-up without insertion

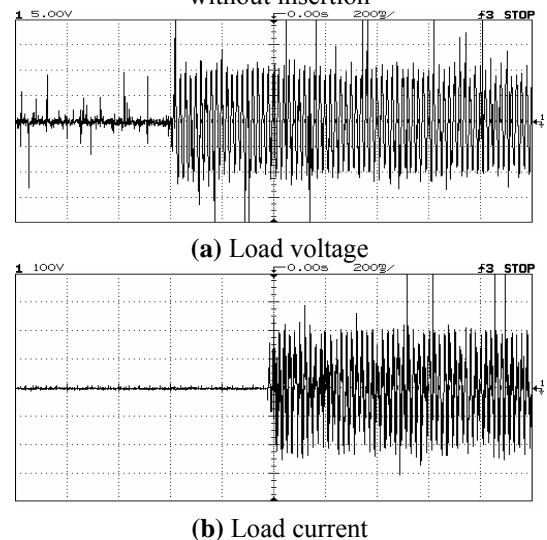
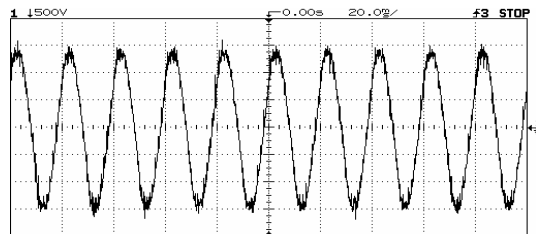


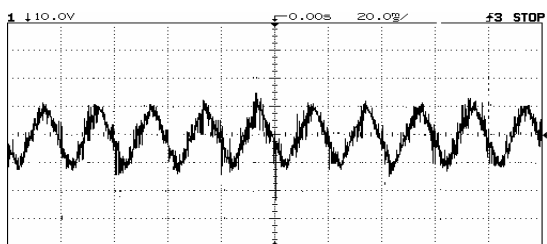
Figure (12) load voltage and current during Run-up with insertion

6.2. Steady-State Characteristics

Figures (13) and (14) show the experimental waveforms of load voltage and current with and without insertion during steady-state. It is noticed that the load voltage and current are approximately sinusoidal due to synchronization between the voltages in the two systems.

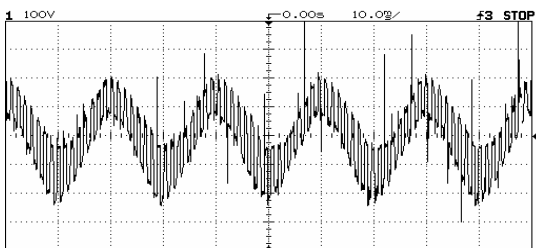


(a) Load voltage

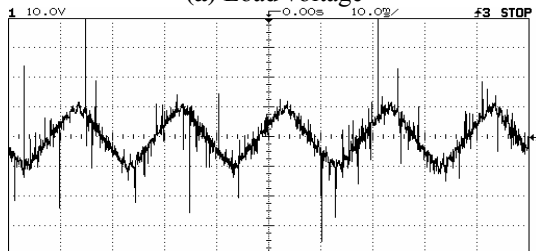


(b) Load current

Figure (13) Experimental steady state load voltage and current without insertion



(a) Load voltage



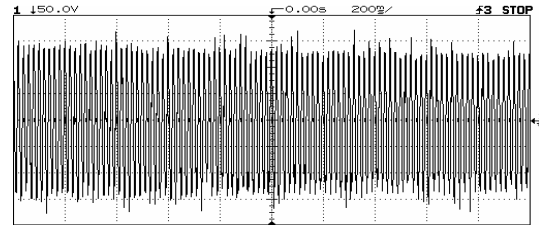
(b) Load current

Figure (14) Experimental steady state load voltage and current with insertion

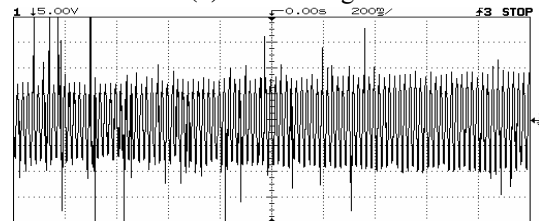
6.3. Load Disturbance

Figure (15) shows the experimental results for the load voltage and current during positive change in load without insertion. Figure (16) shows the experimental results for the load voltage and current during positive change in load with insertion. It is noticed that for the system without insertion, the load

voltage is decreased and load current is increased and take long time about 1.2 sec to reach the steady state value. The load voltage for the proposed system with insertion is constant and the current is increased and take minimum time for reach the steady state value.

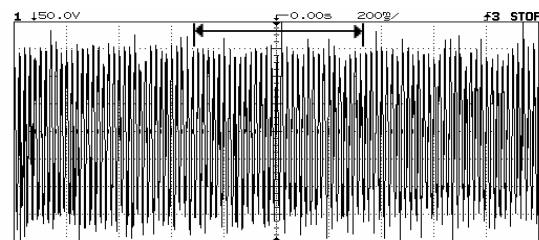


(a) Load voltage

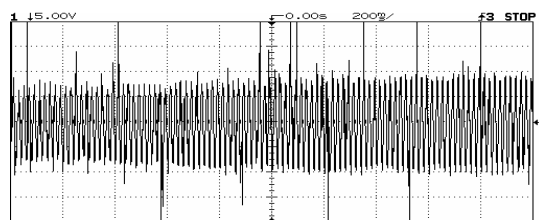


(b) Load current

Figure (15) Experimental load voltage and current during load disturbance without insertion



(a) Load voltage



(b) Load current

Figure (16) Experimental load voltage and current during load disturbance with insertion

7. CONCLUSION

The proposed system uses controlled capacitor as a series compensator to improve the input power factor. With PI controller the system operates as a voltage controller to regulate the load voltage without discontinuity of the supply current. The capacitor value affects the system performance when the capacitor value is greater than the total system reactance, the proposed system operates as a boost voltage regulator.

The system can also be used as a series compensation for voltage sag mitigation. The injection voltage can be changed by changing the duty ratio, the load voltage can be kept at a constant value at starting and at load disturbance.

The simulation results for both open and closed loop voltage control are given and proved to yield good agreement when compared with the experimental results.

8. REFERENCES

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APPENDIX

The System Parameters

Static load

R_L	load resistance	= 35 Ω
L_L	load inductance	= 0.155 H
R_S	supply resistance	= 5 Ω
L_S	supply inductance	= 0.05H
C	max value of controlled capacitance	= 20 μ f

Dynamic load (ac series motor)

R_m	motor resistance	= 10.5 Ω
L_m	motor inductance	= 0.11783mH
J	motor inertia constant	= 0.0015 Kg.m ²
B	motor friction coefficient	= 0.00001 Nm/rad/s
n	rated motor speed	= 3000 rpm
V	rated motor voltage	= 220 volt
P	rated motor power	= 1/3 hp
I	rated motor current	= 1.9 A